CArbon-14 Source Term CAST

¹⁴C behaviour under repository conditions – application to geochemical based long-term safety analysis for a underground disposal system *Volker Metz, KIT-INE*





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Handling of C-14 in current safety assessments: State of the art.

CArbon-14 Source Term report CAST-2015-D6.1





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PU	Public	X		
RE	Restricted to the partners of the CAST project			
CO	Confidential, only for specific distribution list defined on this document			



containment and isolation of radioactive waste

 \rightarrow deep geological multi-barrier systems



European Council Directive 2011/70/EURATOM of 19 July 2011 establishing a Community framework for the responsible and safe management of spent fuel and radioactive waste:

"Radioactive waste, including spent fuel considered as waste, requires containment and isolation from humans and the living environment over the long term. Its specific nature, namely that it contains radionuclides, requires arrangements to protect human health and the environment against dangers arising from ionising radiation, including disposal in appropriate facilities as the end location point. The storage of radioactive waste, including long-term storage, is an interim solution, but not an alternative to disposal. (...)"

There is still no alternative to final disposal in deep multi-barrier systems for the safe management of high-level radioactive waste. Isolating radioactive waste from the biosphere in a geologically stable environment over periods of several hundreds of thousands of years offers maximum safety, which cannot be guaranteed at present by other concepts

source: Official Journal of the European Union (ABI. L 199, 2. Aug. 2011, p. 48f), http://eur-lex.europa.eu/LexUriServ



Basic concept of multi-barrier disposal systems



Example : Swedish multi-barrier concept (KBS-3)



sources: SKB (2006) Long-Term Safety for KBS-3 Repositories at Forsmark and Laxemar – A First Evaluation, Main Report of the SR-Can project, SKB TR 06-09, Swedish Nuclear Fuel and Waste Management Co., Stockholm; Hedin et al. (2007) NEA-RWM report, NEA No. 6362, Nuclear Energy Agency, Paris, pp 45-56

Technical barrier: UO_x / HLW glass / cement matrix



Engineered barriers: containers for spent nuclear fuel / HLW glass

Thin walled iron "CU1" containers for spent MOX fuel elements and iron "C-overpacks" for HLW coquilles for disposal in claystone (France)



Source: ANDRA 269 VA (Dec 2006): Dossier 2005 Argile, Phenomenological evolution of a geological repository (Dezember 2005), Report Series ; T. Hassel et al. (2014) Behälterdossier, ENTRIA, Leibniz Universität Hannover, Version 0.2





Thick walled cast iron container with inner steel container for spent nuclear fuel elements and HLW coquilles for disposal in rock salt (for example Germany) Nodular iron (a kind of cast iron) container with 5 cm thick copper liner as chemical barrier against corrosion for disposal in crystalline rock (for example Sweden and Finland)



Sources: GRS, Endlagerung wärmeentwickelnder Abfälle in Deutschland, GRS-247, 2008; 9. Projektstatusgespräch BMBF/BMWI-geförderter FE-Vorhaben zu Entsorgung gefährlicher Abfälle in tiefen geol. Formationen, 2010; SKB, Technical Report, TR-01-03, December 2000

International concepts for final disposal of radioactive waste





short-lived LLW - shallow land disposal

• at sites with *clay-rich aquicludes* for reasonable protection of groundwater (Czechia, France, Finland, Japan, Sweden, Spain, United Kingdom, USA ...)

LLW / ILW – final disposal in deep geological formations

- rocks with argillaceous overburden (Canada, Germany)
- granite (Hungary)
- bedded salt formations (USA)
- salt diapirs (Germany)
- clay rock or marl (Switzerland)

HLW – final disposal in deep geological formations



- granite / granitoides (Finland, Sweden, Spain and Argentina, China, Czechia, Hungary, India, Japan, Korea, Lithuania, Russia, Slovakia, South Africa, United Kingdom)
- salt (Germany, Lithuania, Netherlands, Romania, Russia, USA)
- *clay rock*, plastic (Belgium , Netherlands)
- *clay rock*, solidified (Argentina, Bulgaria, France, Germany, Hungary, Italy, Japan, Lithuania, Switzerland, Slovenia, Spain, United Kingdom

SNF and HLW-glass disposal in rock salt (Germany, Netherlands)



- disposal in depth of 500 to 800 m
- very high plasticity →
 "complete isolation" possible
- host rock posses extremely low permeability (except anhydrite zones)
- thick-walled cask iron / steel container
- back-filling with crushed rock salt
- reference case: no water access
- less probable scenarios: water access due to failure of shaft sealing etc.

Sources: J. Grupa, E. Rosca-Bocancea & H. Meeussen (2015) NRG contribution to D6.1 in Handling of C-14 in current safety assessments: State of the art. CArbon-14 Source Term (CAST). Thermal Simulation of Drift Emplacement (TSDE) 1990 – 2000, Asse II, 800 m level; Bollingerfehr, W. et al. (2011) EUGENIA, DBE-Technology, BGR; FKZ 02 E 10346

Rock salt : heat conductivity and convergence



Source: Thermal Simulation of Drift Emplacement (TSDE) 1990 – 2000, Asse II, 800 m level

Potential migration paths in rock salt : anhydrite bands



rock salt (Na3) with anhydrite bands, Schachtanlage Asse II

SNF disposal in crystalline rock (Finland, Sweden, Canada)

 $10 \mu m$

bentonite plugs



- advective water transport → bentonite as barrier against water access and radionuclide migration
- nodular iron with 5 cm thick Cu liner as chemical barrier against corrosion

sources: SKB (2006) Long-Term Safety for KBS-3 Repositories at Forsmark and Laxemar – A First Evaluation, Main Report of the SR-Can project, SKB TR 06-09, Swedish Nuclear Fuel and Waste Management Co., Stockholm; Hedin et al. (2007) NEA-RWM report, NEA No. 6362, Nuclear Energy Agency, Paris, pp 45-56; Pastina, B. & Hellä, P.: Expected evolution of a spent fuel repository in Olkiluoto, Posiva 2006-05, December 2006

SNF disposal in crystalline rock (Czech Republic)

- fractured granitoid rock with advective water transport → bentonite as barrier against water access and radionuclide migration
- canister consists of an outer layer of carbon steel (which will corrode very slowly under anaerobic conditions) and a second inner layer of stainless steel (which will corrode at an almost negligible general corrosion rate and exhibit a low tendency to local corrosion under anaerobic conditions)



source: Antonín Vokál (2015) SURAO contribution to D6.1 in Handling of C-14 in current safety assessments: State of the art. CArbon-14 Source Term (CAST)

Montmorillonitic smectite: main constituent of claystone / bentonite



chemical analysis (wt %)				
SiO2	61			
AI2O3	20			
TiO2	<1			
Fe(III) as Fe2O3	3			
MnO	<1			
MgO	3			
CaO	1			
Na2O	2			
К2О	<1			
loss on ignition	11			
total	100			

$M_{0.66}[Mg_{0.66}AI_{3.34}][Si_8]O_{20}(OH)_4 \cdot (H_2O)_n$



SNF/HLW and LLW/ILW in Callovo-Oxfordian clay rock (France)



SNF disposal in Boom Clay (Belgium, Netherlands)



SNF and HLW-glass disposal in Opalinus clay (Switzerland)



Properties of rock types

Properties	rock salt	clay / clay rock	crystalline rock
heat conductivity *	high	low	medium
* temperature load	high	low	high
** permeability	impermeable	very low	permeable
** sorption capacity	very low	very high	medium
** solubility	high	very low	very low
* mechanic stability	medium	medium	high
* plastic behavior	viscose	plastic	brittle
* excavation stability	convergence	very low	low (fractured)

Source: Table after BGR (2007) "Untersuchung und Bewertung von Regionen mit potenziell geeigneten Wirtsgesteinsformationen" Hannover / Berlin

Primary safety functions assigned to engineered anthropogenic and

natural geogenic parts of the repository system

Rock salt contains waste + canister retains / delays release for limited time

Clay retains / delays radionuclide release + canister retains / delays release for limited time



source: J. Grupa, E. Rosca-Bocancea & H. Meeussen (2015) NRG contribution to D6.1 in Handling of C-14 in current safety assessments: State of the art. CArbon-14 Source Term (CAST)

Long-term safety analysis as component of safety case

IAEA / OECD-NEA definitions



International Atomic Energy Agency



Agence pour l'énergie nucléaire Nuclear Energy Agency

The safety case is an integration (a synthesis) of evidences, analyses and arguments that describe, quantify and substantiate the safety, and the level of confidence in the safety, of the geological disposal facility

Safety assessment is a crucial part of the safety case. It is the process of systematically analyzing the hazards associated with the facility and the ability of the site and designs to provide the safety functions and meet technical requirements

Safety Analysis Model Chain:

- Container and waste degradation → radionuclide release (leaching, dissolution of waste)
- Near-field source term \rightarrow including radionuclide <u>retention</u> by engineered barriers
- Transport and retardation in the geosphere
- Biosphere modelling (e.g. dilution in near-surface waters and aquifers, up-take through food chain, exposure) → Annual individual dose mSv/a

Transport processes under repository conditions (near-field)

C-14 and other mobile

After breaching of the container, radionuclides may be released from the waste after contact with water

Transport and retardation of radionuclide species radionuclides in the engineered barriers (i.e. corroded container + backfilling)

Release into geosphere

Radionuclide transport occurs in most cases in aqueous solution (pore and ground water) e.g. dissolved ¹⁴CO3²⁻ or ¹⁴CH₃COO⁻

In some cases radionuclides are released as gases e.g. ¹⁴CH4

Spent nuclear fuel matrix, cladding and Fe-based canister

Technical barrier:

Geo-engineered barrier: backfill / buffer material

Relevance of ¹⁴C in long-term safety analyses

¹⁴C is relatively fast released from spent nuclear fuel (¹⁴C belongs to Instant Release Fraction) as well as fast released from metallic parts of fuel assemblies

Retention of ¹⁴C by container material, geoengineered depends both on chemical speciation of ¹⁴C and on geochemical milieu in repository system (i.e. pH, eH, fluid composition, properties of barrier materials)

¹⁴C is expected to migrate through multi-barrier system as dissolved species (e.g. ¹⁴CO3²⁻ or ¹⁴CH₃COO⁻) or as gases (e.g. ¹⁴CH4)



Since knowledge on chemical speciation of ¹⁴C and reliable knowledge on retention mechanisms is rather **poor**, a significant ¹⁴C release and negligible ¹⁴C retention is assumed in most safety assessments \rightarrow

¹⁴C is one of the radionuclides that produces the highest releases from the near field to the geosphere, especially in the first thousands years, according to long-term safety analyses for repositories in clay / clay stone and crystalline rocks

source:

Example: Long-term safety analysis of SKB (Sweden)

Estimate of effective doses with contribution of C-14 in probabilistic calculations for a normal evolution scenario in a SNF repository in granite \rightarrow calculated dose dominated by long-lived fission, activation and decay products (C-14, Cl-36, I-129, Nb-94, Pb-210, Ra-226, Se-79) and to less extent by actinides

Mean <u>annual</u> effective dose (µSv), i.e. mean effective dose rate (µSv/year)

source: Wikberg (2012) ATW Int'l Journal Nucl Power 57, 102-105



Example: Long-term safety analysis of ENRESA (Spain)

Mean release rates from the near field in probabilistic calculations for a normal evolution scenario in a SNF repository in granite. Only C-14 transport as solute is considered.



source: Miguel Cuñado Peralta (2015) ENRESA contribution to D6.1. Handling of C-14 in current safety assessments: State of the art. CArbon-14 Source Term. CAST-2015-D6.1

Example: Long-term safety analysis of ENRESA (Spain)

Estimate of effective doses with contribution of C-14 in probabilistic calculations for a normal evolution scenario in SNF repository in clay stone. Only C-14 transport as solute is considered.



source: Miguel Cuñado Peralta (2015) ENRESA contribution to D6.1. Handling of C-14 in current safety assessments: State of the art. CArbon-14 Source Term. CAST-2015-D6.1

Example: Long-term safety analysis of SURAO (Czech Republic)

Mean release rates from the near field in probabilistic calculations for a normal evolution scenario in a SNF repository in granite.



source: Antonín Vokál (2015) SURAO contribution to D6.1. in Kendall et al., Handling of C-14 in current safety assessments: State of the art. CArbon-14 Source Term. CAST-2015-D6.1

Example: Long-term safety analysis of SURAO (Czech Republic)

Estimate of effective doses with contribution of C-14 in probabilistic calculations for a normal evolution scenario in a SNF repository in granite.



source: Antonín Vokál (2015) SURAO contribution to D6.1. in Kendall et al., Handling of C-14 in current safety assessments: State of the art. CArbon-14 Source Term. CAST-2015-D6.1

Example: Long-term safety analysis of NAGRA (Switzerland)

Estimate of effective doses with contribution of C-14 in probabilistic calculations for a normal evolution scenario in a spent nuclear fuel (SNF) repository and low-/intermediate level waste

(L/ILW) repository in clay stone. 10^{2} 10^{1} Typical natural radiation exposures in Switzerland 10^{0} 10^{-1} Regulatory guideline: 0.1 mSv a⁻¹ Dose [mSv a⁻¹] 10^{-2} **SNF** 10^{-3} 10^{-4} 10^{-5} ¹⁴C(org 36 CI 10^{-6} 1281 10^{-7} 10^{-6} NSA 10^{-9} 10^{3} 104 10^{5} 10^{2} 10^{5} 10^{7} 10^{2} 10^{1} Typical natural radiation exposures in Switzerland 10^{0} 10^{-1} Regulatory guideline: 0.1 mSv a⁻¹ Dose [mSv a⁻¹] 10^{-2} L/ILW 10^{-3} Effective dose 10^{-4} rate in 10^{-5} biosphere 10^{-6} $^{36}\mathrm{Cl}$ 10^{-7} (Sv/year) 79Se 10^{-8} C(org) 10^{-9} source: Johnson et al. (2004) NAGRA NTB 04-03 10^{3} 10^{6} 10^{2} 10^{5} 10^{T} 10^{4}

Time [a]

Simplified thermodynamic stability fields of ¹⁴C compounds at 25°C



however other organics species are not included (mixed oxidation states)

Under repository conditions, ¹⁴C is released from spent nuclear fuel, cladding (Zircaloy) and other metallic parts of fuel assemblies as

- organic solutes (e.g. methanol, ethanol, formaldehyde, acetaldehyde, formate, acetate)
- aqueous inorganic species (e.g. ¹⁴CO3²⁻, H¹⁴CO3⁻)
- organic gases (e.g. ¹⁴CH4)
- inorganic gases (e.g. ¹⁴CO₂)
- \rightarrow defining the ¹⁴C source term





Transport / retardation processes under repository conditions

After breaching of the container, radionuclides may be released from the waste after contact with water

Transport and retardation of radionuclides in the engineered barriers

= chemical interactions with ground-water / porewater (e.g. $Ca_{2+} + {}^{14}CO_{3^{2-}} \rightarrow$ precipitation of calcite) ruled by solubility phenomena

and **biotransformation** of organic species into ¹⁴CH4, ¹⁴CO2

and chemical interactions with solid phases (corroded metal, bentonite, concrete, host rock)

- isotopic dilution, e.g. $Ca^{12}CO_3 \rightarrow Ca^{14}CO_3$
- sorption, surface precipitation, solid solution formation, incorporation

C-14 and other mobile radionuclide species

Basic concept for concentration limitation due to solubility phenomena



Basic concept for migration and retention in geo-engineered / geological barriers



biotic degradation of organic ¹⁴C compounds into ¹⁴CH₄ and ¹⁴CO₂



- aerobe respiration $CH_2O + O_2 = CO_2 + H_2O$
- denitrification $CH_2O + 4/5 H^+ + 4/5 NO_3^- = CO_2 + 2/5 N_2 + 7/5 H_2O$
- Fe³⁺ reduction $CH_2O + 8 H^+ + 4 Fe(OH)_3 = CO_2 + 4 Fe^{2+} + 11 H_2O$
- SO_4^{2-} reduction $CH_2O + \frac{1}{2}H^+ + \frac{1}{2}SO_4^{2-} = CO_2 + \frac{1}{2}HS^- + H_2O$
- methanogenesis $C_6H_{10}O_5 + H_2O = 3CO_2 + 3CH_4$

¹⁴C behaviour under repository conditions – application to long-term safety

analyses for SNF / HLW repositories in clay / claystone (BE, CH, NL)

Conservative approaches to simulate ¹⁴C behaviour:

- ¹⁴C released from SNF is assumed to be in **organic** form; transport in Opalinus Clay and Boom Clay is dominated by **diffusion**, whereas advective flow and gas transport are considered negligible
- no sorption is considered for organic forms of ¹⁴C (NAGRA)
- ¹⁴C is assumed to be not retarded at all (ONDRAF-NIRAS)
- Still, since diffusion rate is very slow and migration path from deep underground repository to biosphere is rather long, virtually all ¹⁴C will decay in Boom Clay host rock (NRG)





source:

¹⁴C behaviour under repository conditions – application to long-term safety

analyses for HLW repository in clay stone (FR)

Conservative approach to simulate ¹⁴C behaviour: Migration of complete ¹⁴C inventory as gas without any retention; conservative approach chosen by ANDRA due to lack of knowledge on chemical ¹⁴C behaviour under repository conditions

Alternative approach to simulate ¹⁴C behaviour (ANDRA): Taking into account migration of complete ¹⁴C inventory as dissolved inorganic species; considering migration by diffusion, advection and dispersion and sorption of inorganic ¹⁴C species in bentonite, concrete and claystone



source:

14C behaviour under repository conditions – application to long-term

safety analyses in crystalline rock (SF, CZ)

Diffusion through bentonite backfilling and advective transport of dissolved species in crystalline bedrock considered

14C speciation may change due to reactions either inside the repository or while migrating along the bedrock fractures

Due to related uncertainties, 14C is conservatively assumed to be released in organic gaseous form in alternative scenario (FORTUM)

Diffusion coefficients for bentonite as well as sorption coefficients for bentonite and granite are estimated (SURAO)



source:

Complete isolation in "normal evolution scenarios" of long-term safety

analyses for repositories in rock salt (DE, NL)

"In the case of disposal in rock salt, the waste is completely enclosed by several hundred meters of dry rock salt. Consequently, **all C-14 will decay in the facility**. The displacement of air from the mine (potentially including C-14), caused by the convergence of the rock salt has not yet been taken into account." (NRG)

"Crushed salt backfill is expected to be compacted over time by convergence of the host rock to achieve a sufficiently high hydraulic resistance to avoid inflow of brines into the repository. Plugs and seals **must** provide their sealing function during the early post closure phase, until the compaction of the backfill is adequate and the permeability of the backfill is sufficient low. (...) According to the regulations, the waste containers (...) **must** be designed to avoid the release of radioactive aerosols for a period of 500 years. No dissolved radionuclides are released from the isolating rock zone during the whole reference period." (GRS)



Different results for less probable scenarios: water access due to failure of shaft sealing etc.

source:

- ¹⁴C is relatively fast released from spent nuclear fuel as well as fast released from metallic parts of fuel assemblies
- Retention of ¹⁴C by container material, geo-engineered barriers and geological barriers depends both on chemical speciation of ¹⁴C and on geochemical milieu in repository system
- ¹⁴C is expected to migrate through multi-barrier system as dissolved species or as gases
- Since knowledge on chemical speciation of ¹⁴C and reliable knowledge on retention mechanisms is rather poor, a significant ¹⁴C release and negligible ¹⁴C retention is assumed in safety assessments for repositories in clay / clay stone and crystalline rock → ¹⁴C is one of the radionuclides that produces the highest releases
- With respect to "normal evolution scenarios", no 14C release is expected from the nearfield of a SNF / HLW repository in rock salt